

09 OCT 2008

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SUBJ: GLASS AWNING SUPPORT SYSTEM

The Glass Awning Support System utilizes stainless steel fittings to construct frameless glass awnings. The system is intended for interior and exterior weather exposed applications and is suitable for use in all natural environments. The system may be used for residential, commercial and industrial applications. The Glass Awning Support System is designed for the following criteria:

The design loading conditions are:

Concentrated load = 50 lbs any direction, any location

Uniform load = 25 psf vertical, live, wind or snow load

The glass awning is not intended to support significant concentrated live loads or personnel. It shall not be used to walk, stand or step on.

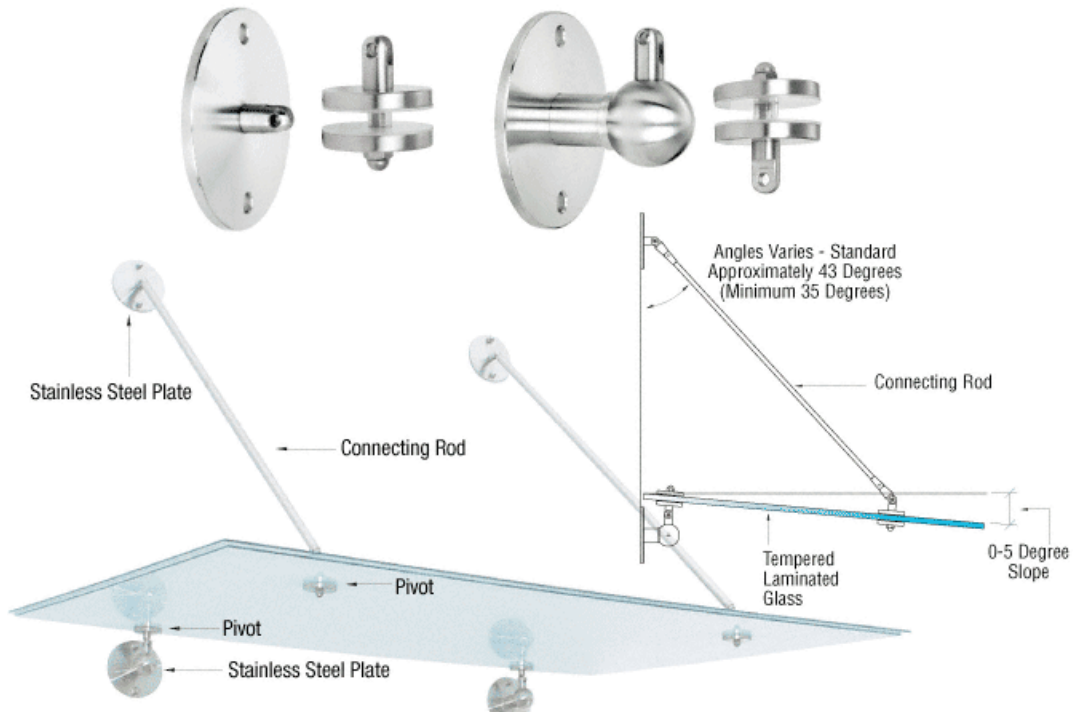
The Awning Support System will meet or exceed all requirements of the 1997 Uniform Building Code, 2000, 2003 and 2006 International Building Codes, and California Building Standards Code. Stainless steel components are designed in accordance with SEI/ASCE 8-02 Specification for the Design of Cold-Formed Stainless Steel Structural Members. Wood components and anchorage to wood are designed in accordance with the National Design Specification for Wood Construction.

Edward Robison, P.E.  
Attachments – Calculations 5 pages

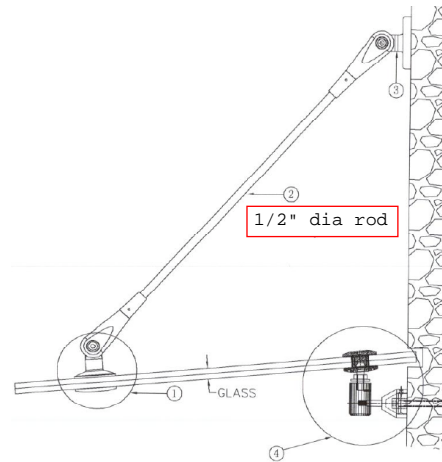
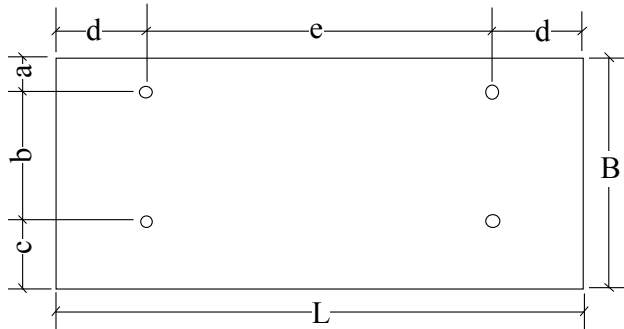
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CRL GLASS AWNING SUPPORT SYSTEM



Support hardware for flat panel awnings such as laminated glass.



Support Rod: 1/2" (12 mm) diameter stainless steel

$$I = 0.00307 \text{ in}^4, \quad A = 0.196 \text{ in}^2$$

$$r = 0.125 \text{ in}$$

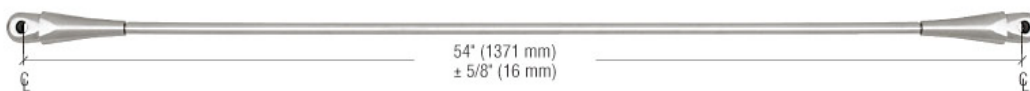
Maximum allowable rod length: 62"

$$kl/r = 0.5 * 62" / 0.125" = 256$$

$$F_a = 12\pi^2 E / [23(kl/r)^2] = 2,121 \text{ psi (allowable compression stress)}$$

$$P_a = 2,121 \text{ psi} * 0.31 \text{ in}^2 = 658\# \text{ compression force (wind uplift)}$$

$$T_a = \phi A_n F_y / 1.6 = 0.85 * 0.196 * 45 \text{ ksi} / 1.6 = 4,686\#$$



Typical hanger rod

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Wall Mount

The wall plate is mounted to the wall with two 3/8" anchors, type dependent on the wall construction. Typical strength of 3/8" anchor is minimum of 500# each for tension and shear.

Reaction from tie bar:

$V = T$  for bar at 45° angle (typical)

$V/1000 + T/1000 = 1.0$

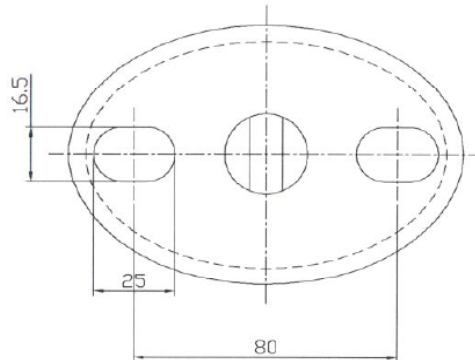
$V = T = 500\#$

Check connector bar strength:

$1/2" \times 1"$  bar  $Z = 0.5 \times 1^2/4 = 0.25 \text{ in}^3$ ,  $F_y = 28 \text{ ksi}$

$M_s = 0.9 \times 0.25 \text{ in}^3 \times 28 \text{ ksi} / 1.6 = 3,937\#"$

okay for 500# tie bar load.



For 4' wide glass:

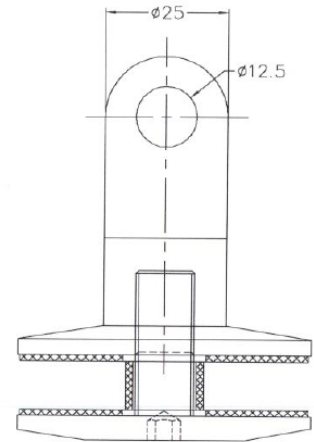
load to rod:

$1/2 \times 4' \times L/2 \times W = LW = 500\#$  allowable

where  $W$  = total uniform load and  $L$  = awning length

For  $W = 31 \text{ psf}$  (6 psf dead load +25 psf live load)

$L_{\text{max}} = 500/31 = 16'$  Limited to 9' by glass strength



Tie rod to glass connection bracket: Connector bar strength is same as for wall bracket therefore okay by inference.

Bottom cap screws into top side bracket:

$1/2"$  threaded stud with minimum  $1/2"$  thread depth.

Strength =  $1.107 \text{ in}^2 \times 0.5" \times 21 \text{ ksi} = 11.6 \text{ k}$  for thread stripping

$T = 0.196 \text{ in}^2 \times 56 \text{ ksi} \times 0.75/1.6 = 5,145\#$  for stud strength

$5/8"$  diameter bracket bar:

$M_s = 0.9 \times 0.0407 \text{ in}^3 \times 45 \text{ ksi} / 1.6 = 1,030\#"$

$H = 1,030\# / 1.125" = 915\#$  doesn't control strength

$1/4"$  connector pin strength:

$V_s = 0.85 \times 25 \text{ ksi} \times 0.049 \text{ in}^2 / 1.6 = 650\# > 630\#$  okay

Bottom Wall Mount

Bottom plate standoff for pivot: assume 630# D+L total load

$M = 630\# \times 2.625" = 1,654\#"$

Bottom plate:  $f_b = 1,654\# / 0.0414 \text{ in}^3 = 39.9 \text{ ksi}$

Top Plate:  $F_b = 42 \text{ ksi}$  per SEI/ASCE 8-02

Top plate standoff for pivot

$M = 630\# \times 0.75" = 473\#"$



$$f_b = 473\# / 0.0123 \text{ in}^3 = 38.5 \text{ ksi}$$

Maximum tributary area per plate:  $630\# / 25 \text{ psf} = 25.2 \text{ sf}$  for bottom plate.

Determine maximum tributary area to support rod:

Maximum rod length is 54" (rod may not be longer for 1/2" diam. based on kl/r limits).

Minimum angle of rod to horizontal is 35°.

From geometry:

$$a+b = 54\text{''}\cos 35^\circ = 44.23\text{''}$$

$$b = 44.23\text{''} - 2.8125\text{''} = 41.4175\text{''}$$

$$h = 54\text{''}\sin 35^\circ = 30.97\text{''}$$

$$c_{\text{max}} = 12\text{''} \text{ so } B_{\text{max}} = 44.23\text{''} + 14\text{''} = 58.23\text{''}$$

For an allowable bar compressive load of 658#

$$\text{Max Vertical load } V = 658\# \cdot \sin 35^\circ = 377\#$$

Uplift from wind check based on 25 psf wind load

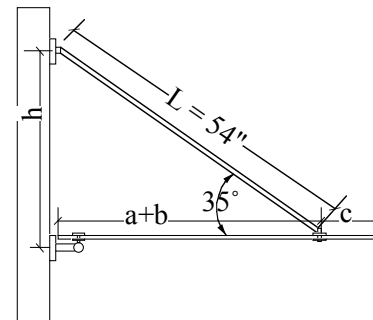
$$U_p = 25 \text{ psf} - 0.6 \cdot 6.5 \text{ psf} = 21.1 \text{ psf}$$

$$\text{Max tributary area} = 377\# / 21.1 \text{ psf} = 17.9 \text{ sf}$$

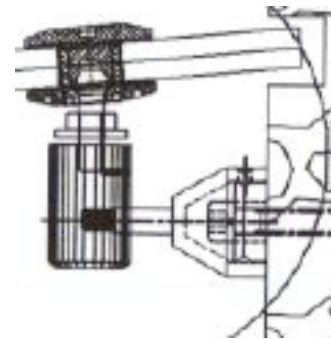
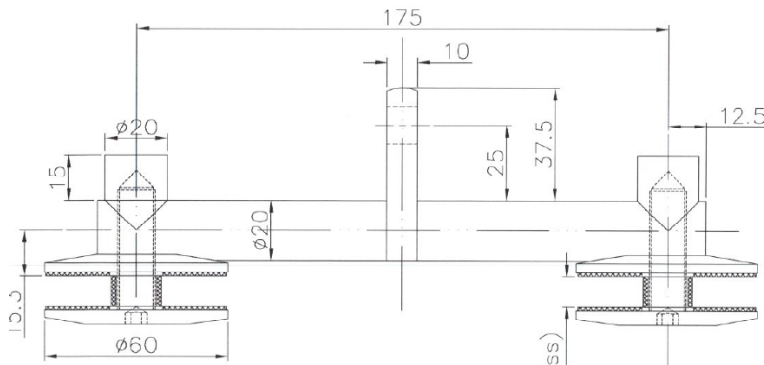
Determine maximum L for B = 58" (4' 10")

$$f = (41.2\text{''}^2 / 2 + 14\text{''} \cdot 48.2\text{''}) / 41.2\text{''} = 37\text{''} = 3.08'$$

$$L = 17.9 / 3.08 \cdot 2 = 11.61'$$



Double bracket (Two adjacent awning panes)



Bending on connection bar between double bracket and wall mount.

$$Z = 0.5^3 / 6 = 0.0208 \text{ in}^3$$

$$M_s = 0.0208 \cdot 50 \text{ ksi} \cdot 0.9 / 1.6 = 586\#\text{''}$$

$$P = 586\#\text{''} / 1\text{''} = 586\#$$

293# allowable for each pane:

Maximum pane size based on 31 psf total load

$$293\# / 31 \text{ psf} \cdot 4 = 37.8 \text{ sf.}$$

## GLASS STRENGTH

Glass is fully tempered 2 layer laminated safety glass conforming to the specifications of ANSI Z97.1, ASTM C 1048-97b and CPSC 16 CFR 1201. The minimum Modulus of Rupture for the glass Fr is 24,000 psi. Glass not used in guardrails may be designed for a safety factor of 2.5 in accordance with ASTM E1300-00.

Adjustment for laminated glass (both layers equal) = 1.7 single layer strength

Allowable glass bending stress:  $24,000/2.5 = 9,600$  psi. – Tension stress

Allowable bearing stress =  $24,000$  psi/ $2.5 = 9,600$  psi.

Bending strength of glass for the given thickness:

$$S = \frac{12 \cdot (t)^2}{6} = 2 \cdot (t)^2 \text{ in}^3/\text{ft}$$

The effective section modulus for 2 layers of 1/4" glass:

$$S = 1.7 \cdot 2 \cdot (0.25)^2 = 0.2125 \text{ in}^3/\text{ft}$$

Allowable bending moment on glass is:

$$M_a = 9,600 \text{ psi} \cdot 0.2125 \text{ in}^3/\text{ft} = 2,040 \text{ #}/\text{ft}$$

Determine critical panel stress from bending:

Longitudinal bending

$$M_l = W \cdot e^2/8 \text{ for uniform load } W \text{ and span } L \text{ or}$$

$$M_l = P \cdot e/4 \text{ for concentrated load } P \text{ and span } L, \text{ highest moment } P \text{ @ center.}$$

$$M_d = W \cdot d^2/2 \text{ at support axis}$$

$$M_d = P \cdot d$$

Transverse bending

$$M_t = L/2 \cdot W \cdot b^2/8$$

$$M_t = L/2 \cdot W \cdot c^2/2$$

For a design load of  $W = 25$  psf (live or wind) or  $P = 50$  lb load

$$e = [(2,040 \text{ #}/12) \cdot 8/25 \text{ psf}]^{1/2} = 7.376' = 88.5'' \text{ Controls for } e$$

$$e = 2,040 \text{ #} \cdot 4/50 = 163'' = 13.6'$$

$$d = [(2,040 \text{ #}/12) \cdot 2/25 \text{ psf}]^{1/2} = 3.68' = 44''$$

$$d = 2,040 \text{ #}/50 = 40.8'' = 3.4' \text{ Controls for } d$$

For maximum  $L = 10'$

$$b = [(2,040 \text{ #}/12) \cdot 8/(5' \cdot 25 \text{ psf})]^{1/2} = 3.30' = 39.6''$$

$$\text{For } b = 41.4175'', L \leq [(2,040 \text{ #}/12) \cdot 8/(3.45^2 \cdot 25 \text{ psf})] \cdot 2 = 9.14' = 109''$$

$$c = [(2,040 \text{ #}/12) \cdot 2/(5' \cdot 25 \text{ psf})]^{1/2} = 1.17' = 14''$$

MAXIMUM PANEL SIZE:

Maximum width B = 4'10" from hanger geometry + cantilever from glass bending

Maximum length L = 10' from glass bending strength

Panel dimensions: Illustrative for typical panel.

Dim	maximum	for 4' x 6' panel
a	= 2-13/16"	fixed length for all panel sizes
b	≤ 41.4175" For L ≤ 109"	35.3/8"
	39.6" ≤ b ≤ 41.4175" For 109" < L ≤ 120"	
c	≤ 14"	9-13/16"
B	= a+b+c ≤ 58"	48"
d	≤ 27"	13-3/8"
e	≤ 88.5"	45-1/4"
L	= 2d+e ≤ 132"	72"

MAXIMUM ALLOWABLE LOADS:

500# per connection point

Total awning pane: 2,000# total dead plus live or snow or wind for support strength.

Limited by glass strength to 1,500# total for 2 ply 1/4" laminated glass (9/16" total).

Double bracket: 586# total, 293# each pane tributary to bracket.

DESIGN CRITERIA

IBC Section 3105 Awnings and Canopies

IBC Section 2404.4